



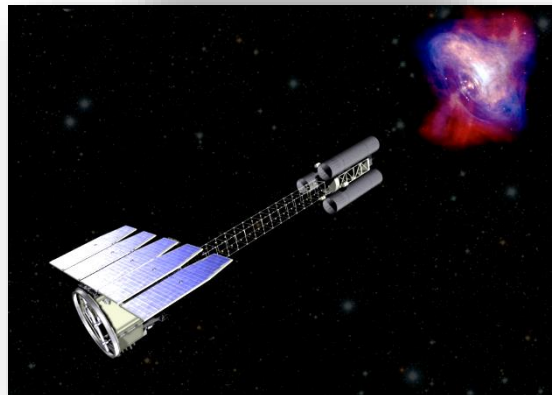
# **X-ray Optics at MSFC**

**Kiranmayee Kilaru**  
**X-ray Astronomy Group**  
**NASA Marshall Space Flight Center**

# X-ray Optics at MSFC

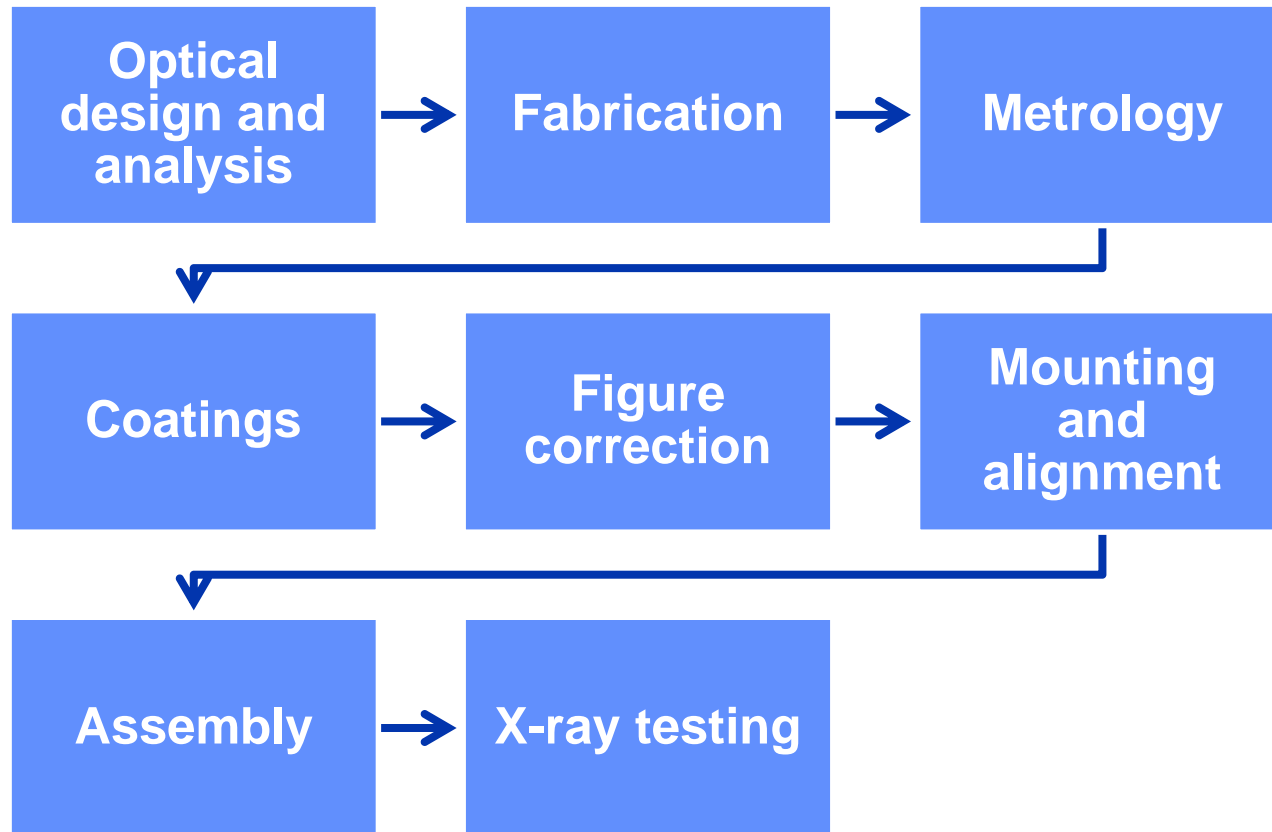


- MSFC has been developing integrated full-shell X-ray optics for ~ 20 years
- Funded initially through ROSES/APRA program
- Fabrication Approach: Electroformed nickel replication
- Optics have been built for satellite, rocket and balloon-borne missions and for various spin-off applications



# X-ray Optics at MSFC

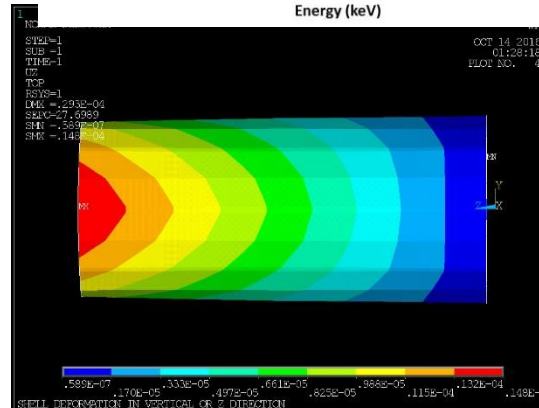
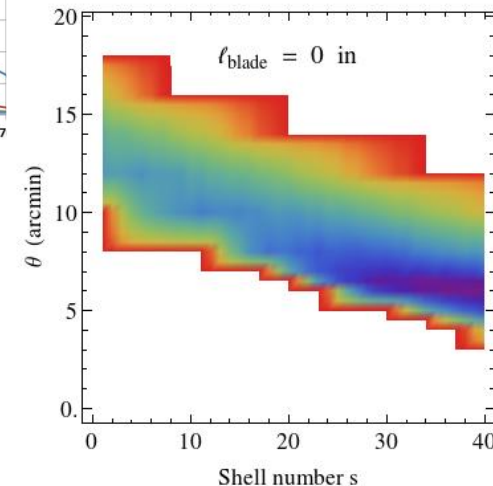
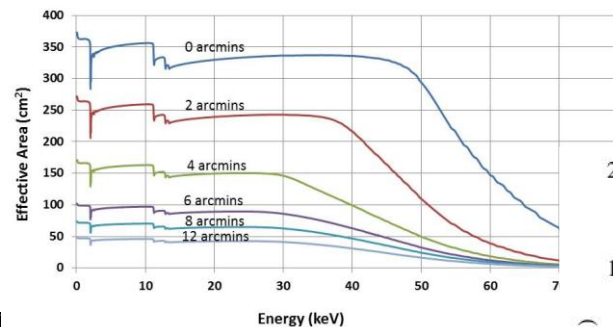
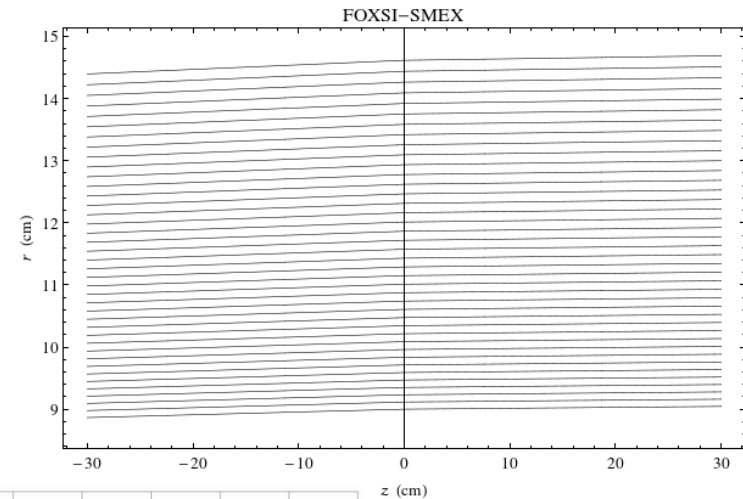
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# Optical Design and Analysis



- Optical configuration – diameter, focal length, segment length, thickness
- Analytical and Monte-Carlo raytracing to characterize the on-axis and off-axis effective area, angular resolution, FOV
- Stray light analysis
- Coatings – Single and Multi-layers
- FEA
  - Mechanical
  - Thermal

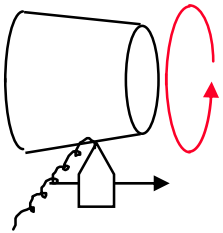


# Electroformed Nickel Replication

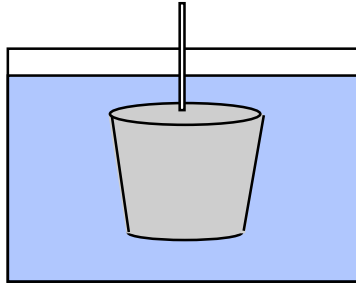


## Mandrel Preparation

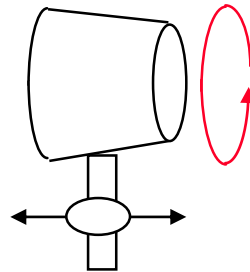
**1. CNC machine mandrel from aluminum bar**



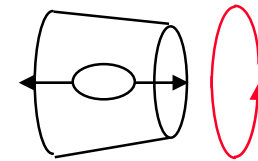
**2. Chemical clean and activation & electroless nickel (EN) plate**



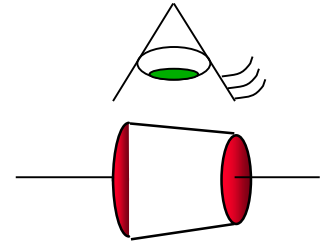
**3. Diamond-turn to few 10s nm surface, sub-micron figure accuracy**



**4. Superpolish to 0.3 – 0.4nm rms finish**

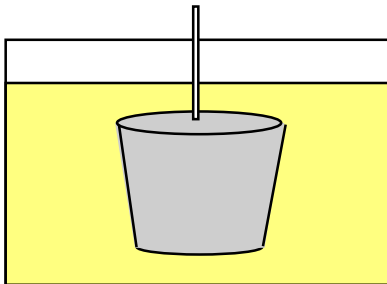


**5. Metrology on mandrel**

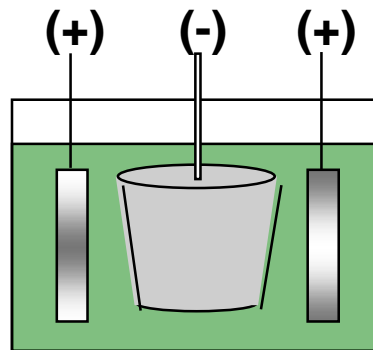


## Shell Fabrication

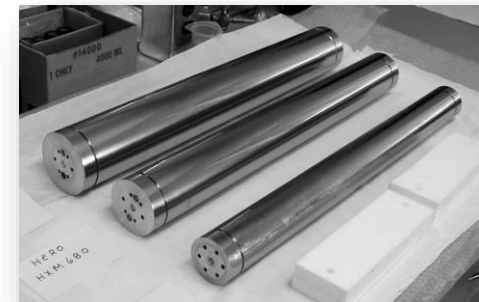
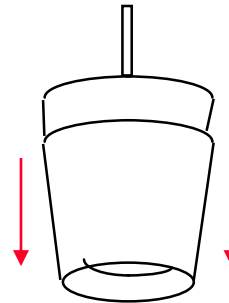
**6. Ultrasonic clean and passivation**



**7. Electroform NiCo shell onto mandrel**



**8. Separate optic from mandrel in cold water bath**





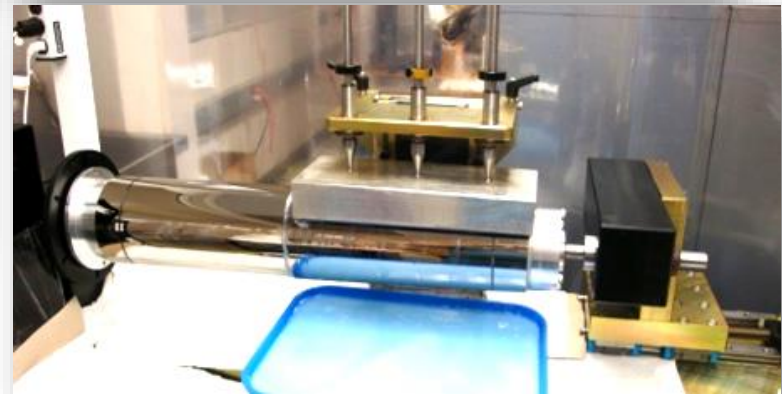
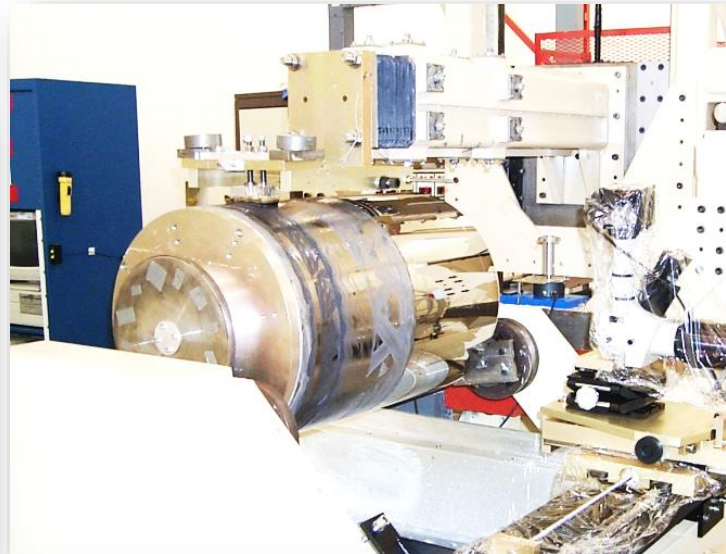
# MSFC Infrastructure



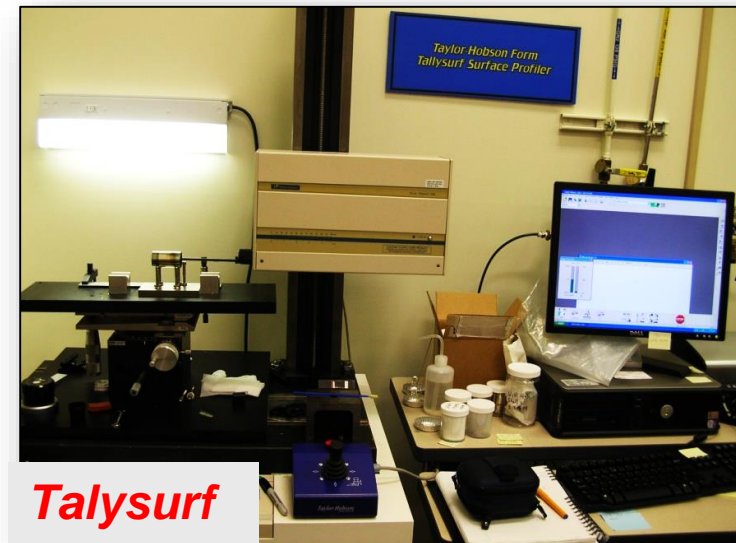
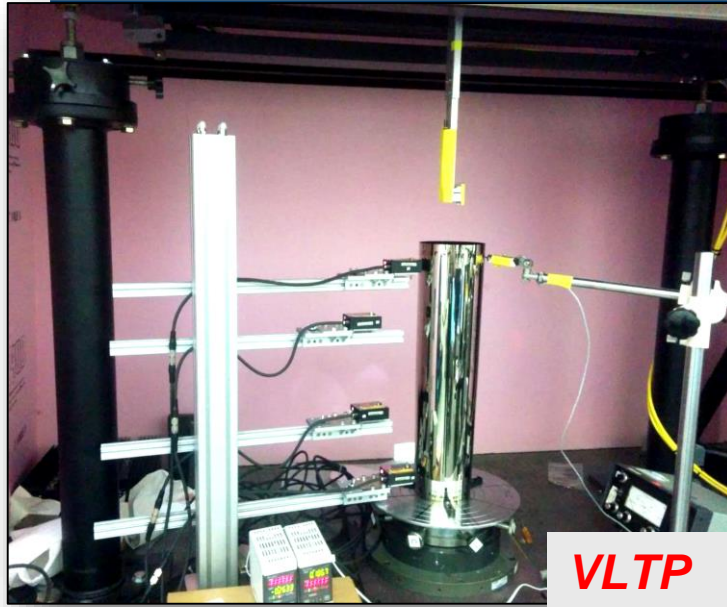
## Mandrel Diamond-Turning



## Mandrel Polishing



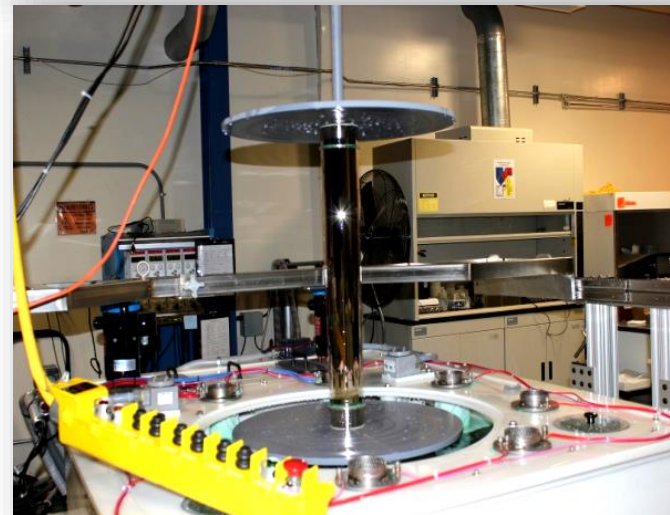
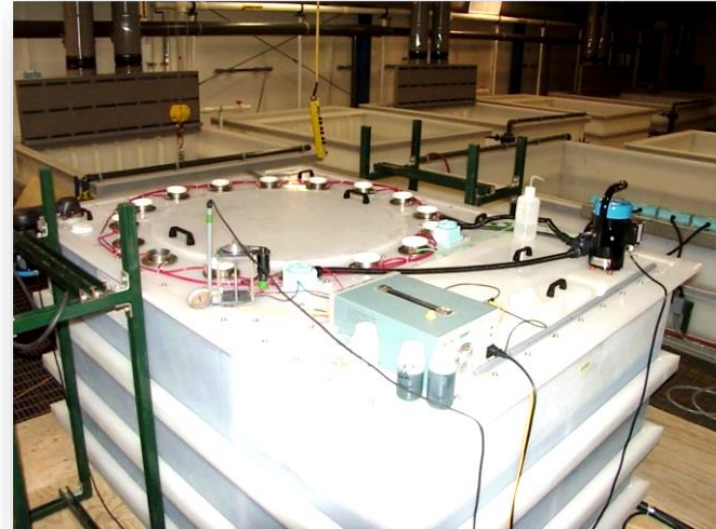
# MSFC Infrastructure - Metrology



- Surface profile – Long Trace Profiler ( $>2\text{mm}$  spatial wavelength), Form Talysurf surface profiler ( $< 120\text{ mm}$ ), Zygo interferometer (mandrel figure metrology)
- Surface roughness - Zygo NewView (spatial sampling range 0.04 to 11.8 microns)
- Circularity - Coordinate Measuring Machine
- Coating characterization - XRR (X-ray reflectometer for density, thickness and roughness), Step Profiler



# MSFC Infrastructure - Replication



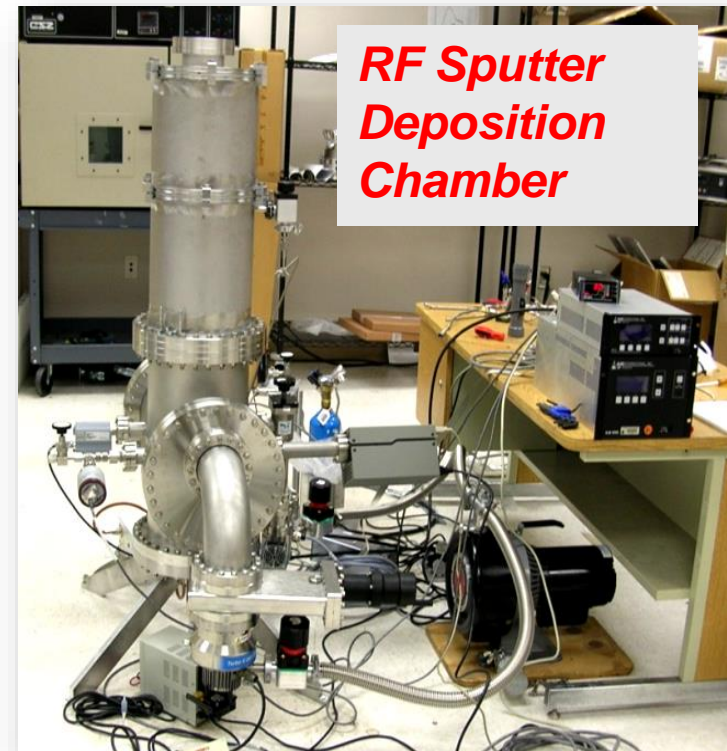


# MSFC Infrastructure - Coatings

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- Custom designed coating chambers for full-shell optics
- RF and DC magnetron sputter deposition
- Underway – Multilayer deposition chamber
- Active research in In-Situ stress measurement and analysis

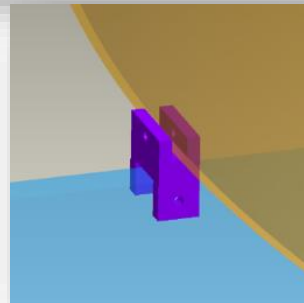
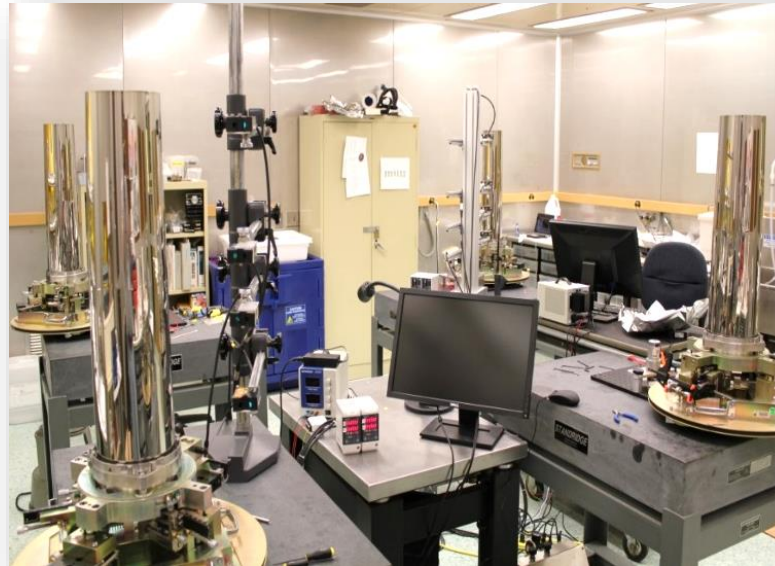


# MSFC Infrastructure – Alignment & Assembly

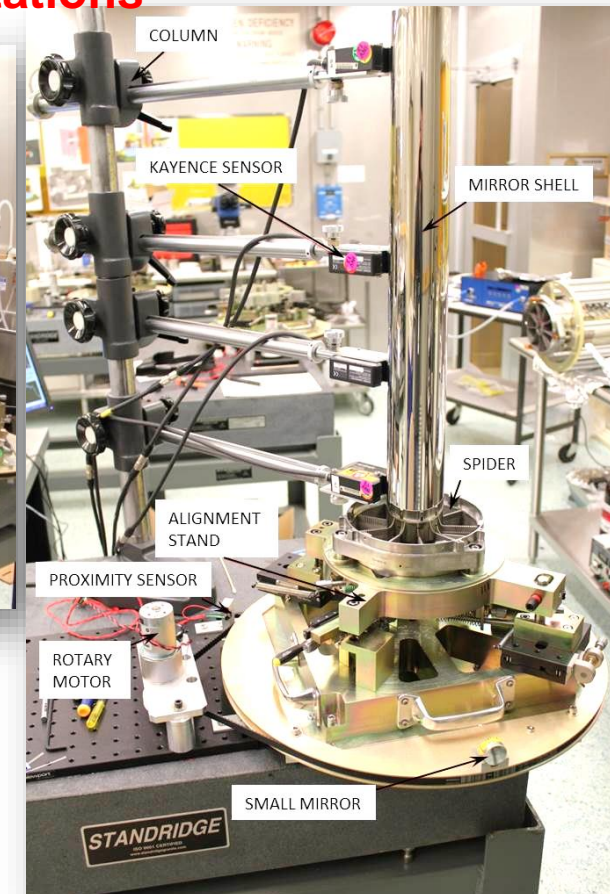


## Mirror shell alignment and installation stations

- Shells are glued from one end – less weight for the support system, less obscuration
- General approach: Convert radial displacement into azimuthal one
- The use of the clips minimizes the distortions due to epoxy shrinking

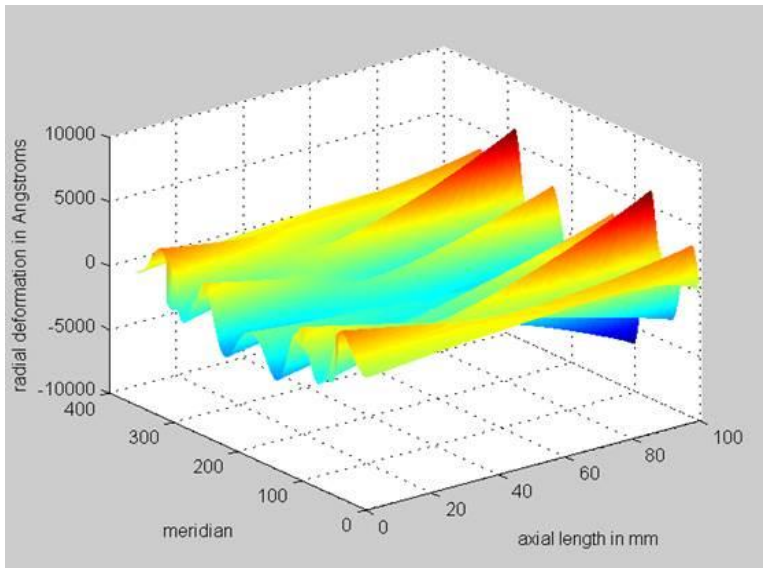


*Pre-glued clips minimize the distortions due to epoxy shrinkage*

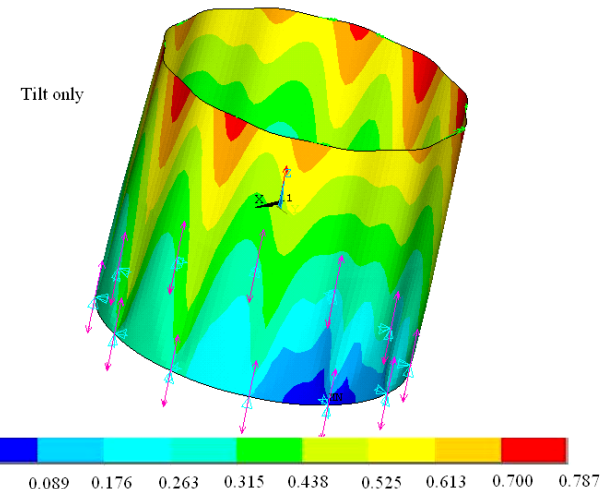


Mikhail Gubarev et.al; Alignment system for full-shell replicated x-ray mirrors. Proc. SPIE 7360, EUV and X-Ray Optics: Synergy between Laboratory and Space, 73600A (April 30, 2009); doi:10.1117/12.823848.

# Alignment & Assembly - FEA



- Sensitivity to radial displacements
- Any radial distortion on one edge of the shell leads to distortions on other end of the shell



*Deformation maps for the 34 cm diameter, 60 cm length monolithic shell supported with 12 points at the bottom of the mirror. The shell is tilted by 1 microradian. The distortion scale is in microns.*

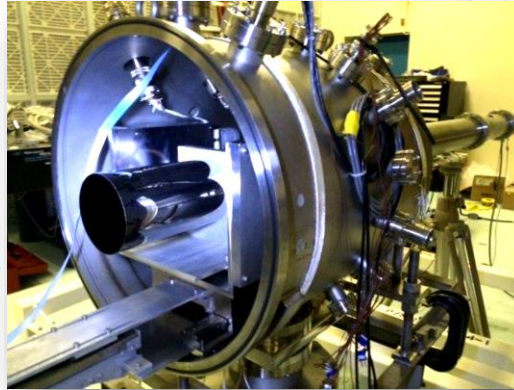


# MSFC Infrastructure – X-ray Testing



## Straylight test facility (SLTF) :

- 100m long vacuum tube
- Clean room facility
- Can accommodate mirrors upto 1m diameter
- Pumped with cryopumps upto  $10^{-7}$  torr



## X-ray and Cryogenic facility (XRCF):

- The XRCF is the world's largest optically clean cryogenic and X-ray test facility.
- The facility consists of a 520m-long X-ray guide tube, an instrument chamber, and two clean rooms
- In addition to the large vacuum chamber, the facility has a smaller, more cost-effective cryogenic and cryogenic optical testing chamber for subscale testing of smaller instruments







# Optics Applications

# Full-Shell X-Ray Optics



## Full-shell optics



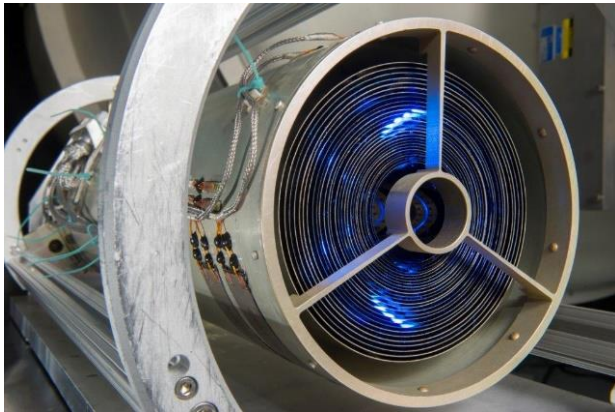
*60 mm length 50 to 100 mm diameter*



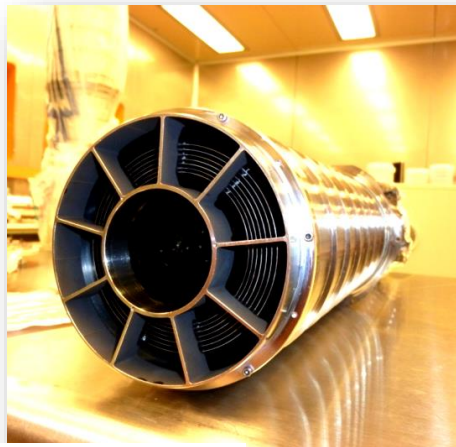
*Down to 50  $\mu\text{m}$  thick*



*Up to 0.5 m diameter*



*Shells nested into a module*



*Down to 0.025 m diameter*

# Replicated X-ray Optic Projects at MSFC



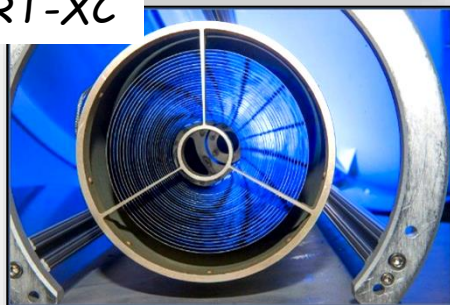
## Astronomical applications

### Past

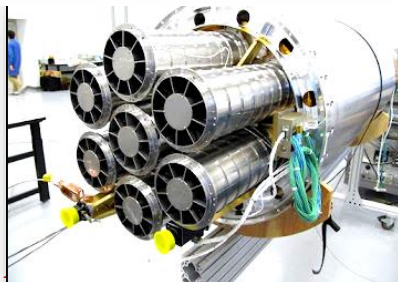
HERO/Super HERO/HEROES



ART-XC

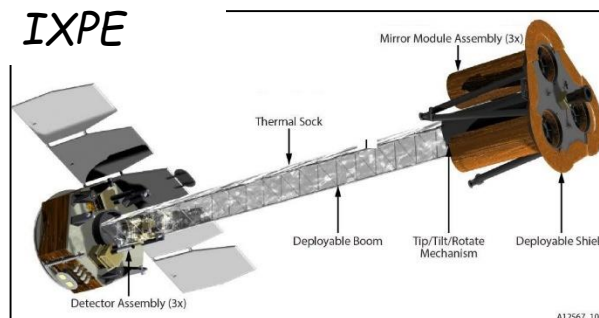


FOXSI/FOXSI-2/FOXSI SMEX

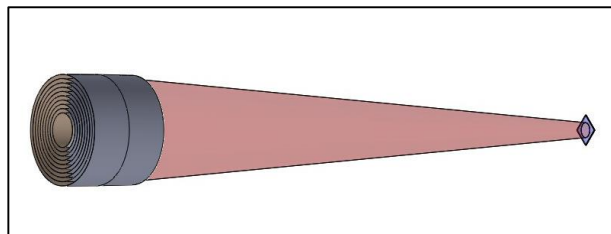


### Current

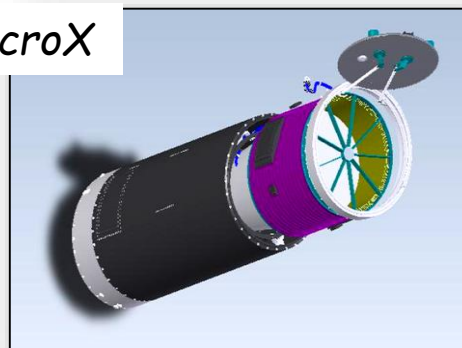
IXPE



MIXO

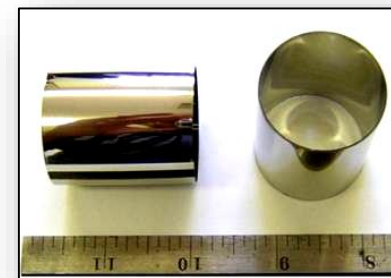


MicroX

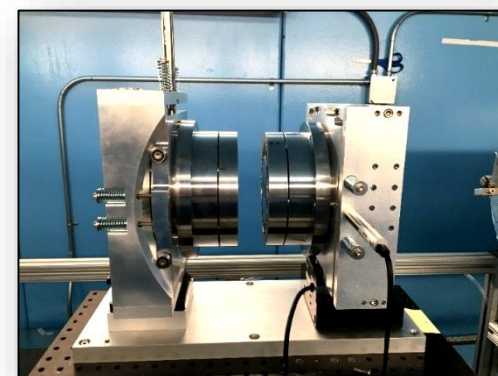


## Non-astronomical applications

Medical imaging



Neutron imaging



X-Ray

# Flight X-ray Optics at MSFC

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	IXPE	ART-XC	FOXSI	HERO
Energy range (keV)	2 - 10	5 - 30	5 - 15	20 - 70
Optics Effective area	1000 cm <sup>2</sup> at 3 keV	≥ 455 cm <sup>2</sup> at 8 keV	150 cm <sup>2</sup> at 10 keV	95 cm <sup>2</sup> at 40 keV, 50 cm <sup>2</sup> at 60 keV
Number of Modules	3	7 (plus 1 spare)	7	8
Focal length (m)	4.0	2.7	2.0	6.0
Number of shells per module	24	28	7	14
Shell diameter range (mm)	162 - 272	50 - 150	76 - 103	50 - 94
Coating	-	Ir	Ir	Ir
Shell thickness (microns)	180 - 250	250 - 325	250	250

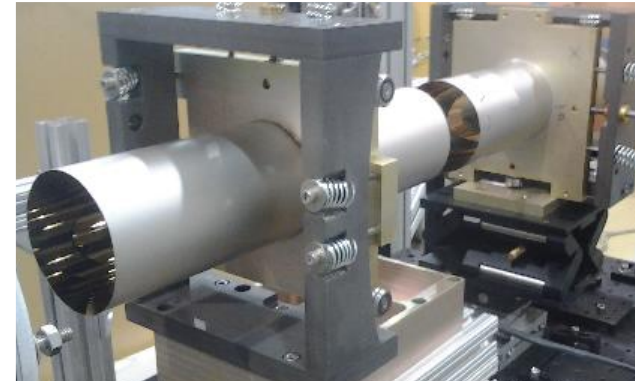


# Spinoff Application: Neutron Microscopy



**Collaboration: NASA MSFC, NIST, MIT**

- Project aims to build the world's first neutron microscope
- Re-envisioning and shaping the future of neutron imaging
- Cold neutron imaging requires similar graze angles as X-rays
- Potential for many commercial applications



*Neutron microscope prototype (2013)  
(shells are made from the parabolic segments  
of existing FOXSI mandrels)*

## *Requirements*

*Mikhail V. Gubarev ; et.al; From x-ray telescopes to neutron focusing. Proc. SPIE 8147, Optics for EUV, X-Ray, and Gamma-Ray Astronomy V, 81470B (September 30, 2011); doi:10.1117/12.897325.*

- *10 shell pairs. Parabola-parabola*
- *1 arc sec FWHM resolution*



# Ongoing Improvements

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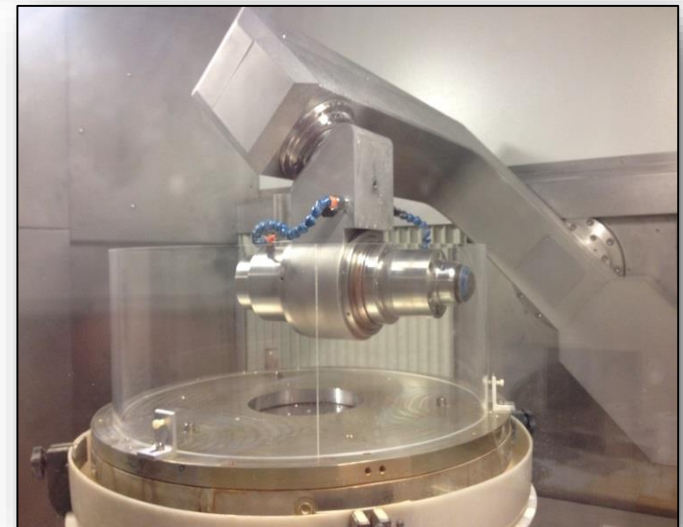
- Typical resolutions are  $\sim 25$  arcsec HPD and  $\sim 4$ - $10$  arcsec FWHM for our production optics
- Efforts underway to improve the resolution include:
  - Better quality mandrels
  - Lower-stress electroforming
  - Direct fabrication (& polishing)
  - Post-fabrication figure correction
  - More precise alignment and assembly
- The near-term goal is a few arcsec HPD and arcsec-level FWHM

# Improved Mandrels: Zeeko Polishing Machine

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- The machine utilizes a “bonnet” technique in which an inflated rubber hemispherical diaphragm supports the polishing medium.
- There are different “bonnet” sizes (20 mm, 40 mm and 80 mm radii of curvature)
- This computer-controlled deterministic polishing processes leads to a high convergence rate.
- Tool path generation (**TPG**) software had to be developed.
- Direct-fabrication of X-ray mirror







# Improved Mandrels: Zeeko Polishing Machine

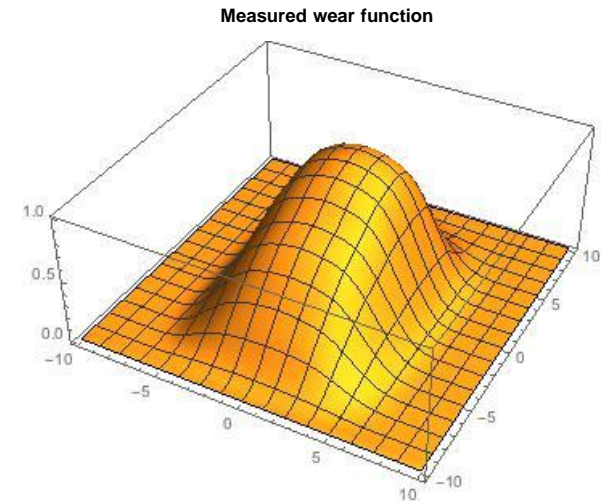
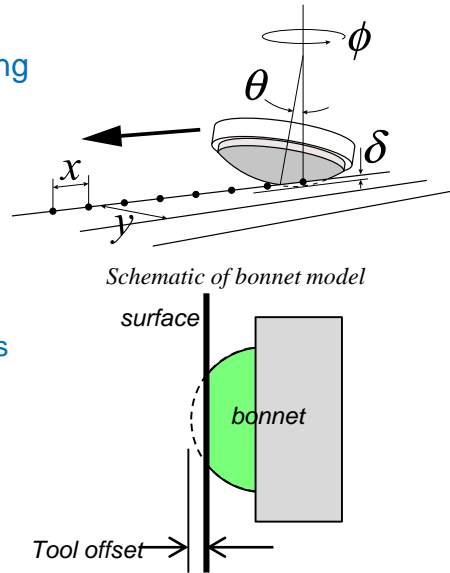
Parametric wear pattern simulation enables a more efficient method of exploring the polishing parameter space.

Wear rate is proportional to :

- Velocity of bonnet depends on
  - Spindle rotation
  - Head attack angles
- Bonnet pressure depends on
  - Internal pressure of bonnet
  - Bonnet structural and mechanical properties

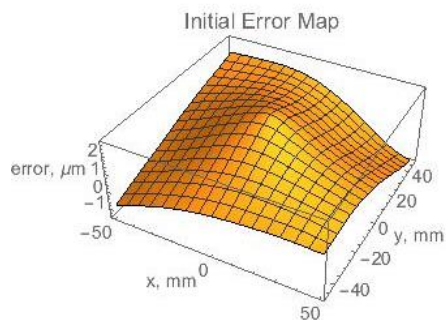
Parameter optimization

Bonnet pressure  
Spindle speed  
Tool Offset



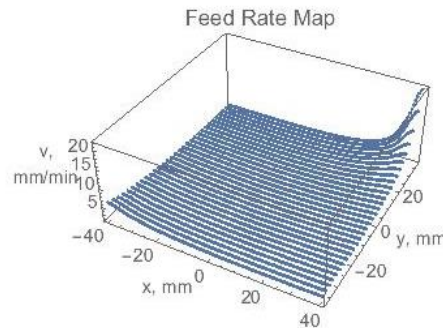
## Wear function characterization

Richardson-Lucy deconvolution algorithm + small nonlinear correction (Tends to generate smoother edge transitions)



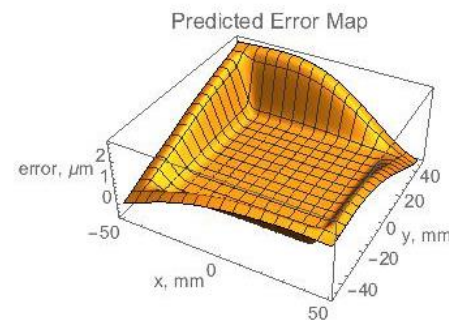
Initial error map derived from metrology data.

RMS slope errors along x-axis are **8 arcsec**



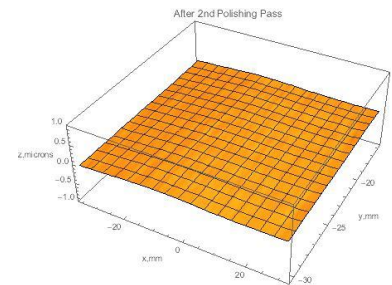
Derived feed rate map.

Feed rates range from 1.35-20 mm/min.



Predicted result of polishing iteration.

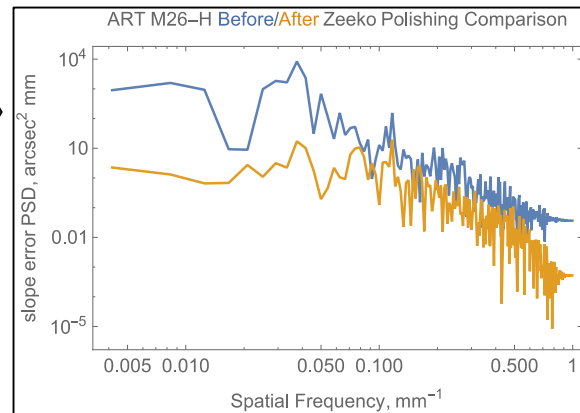
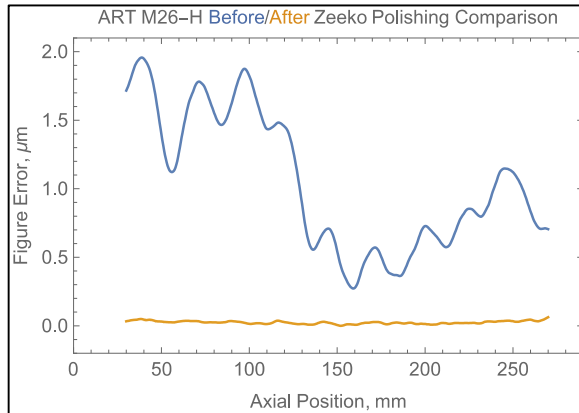
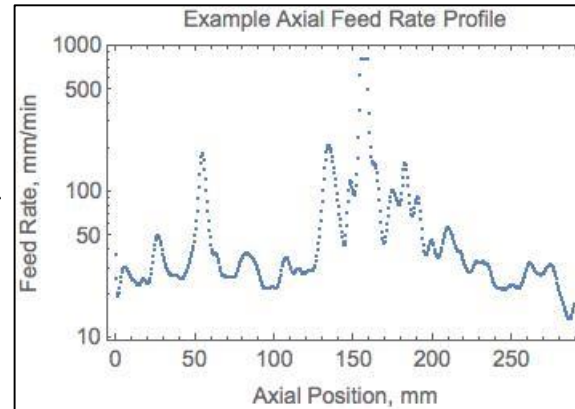
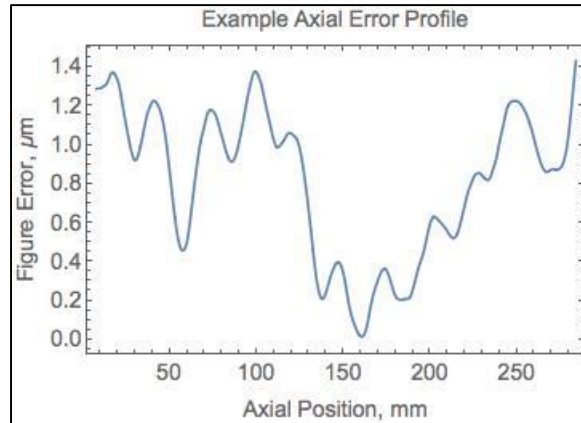
Predicted RMS slope errors are **0.6 arcsec**



Error map derived from metrology data.

RMS slope errors were reduced to **0.5 arcsec**

# Mandrel Demonstration



*Mandrel > 5x  
better than any  
made with  
conventional  
polishing*

	before	after
Figure error (St. Dev.)	500 nm	10.7 nm
Slope error (> 2 cm) (RMS)	6.32 arcsec	0.30 arcsec
Low frequency (> 7 cm) slope error (RMS)	2.66 arcsec	0.09 arcsec
Mid frequency (2-7 cm) slope error (RMS)	5.73 arcsec	0.29 arcsec

# Lower electroforming stresses: Pulsed Plating

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- Reduce stress variations in electroforming through pulsed plating.
  - Periodic reversal of polarity\during electroforming alternates deposition with selective etching, providing a finer grain structure and denser packing.
  - Recent evidence shows that the shells plated this way are very low stress and closer to the mandrel shape than with conventional electroforming.
- Circularity is key for a good FWHM - Pulsed plating of pure nickel recently demonstrated the micron-level circularity necessary for arc-second-level FWHM resolution.

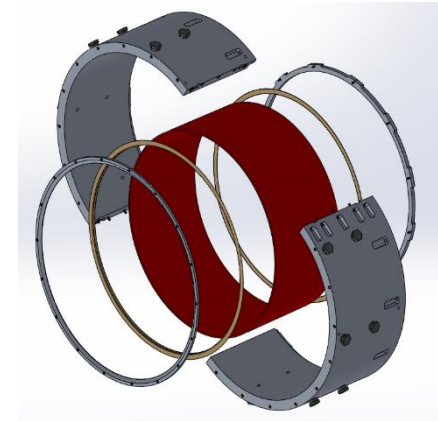


# Full-Shell Direct Fabrication



- Technology development - figure and polish thin x-ray metal optics directly
- Finite-Element Analysis - thickness  $\sim 1.5$  mm will be stable enough to be polished directly
- Metal substrates
  - improve the mechanical stability,
  - Single-point diamond turning instead of grinding process
- Computer controlled deterministic polishing
- In situ metrology system - Phase-Measuring Deflectometry (PMD): Deviations from perfect spacing of fringe pattern measured at multiple phases provides an unambiguous measure of slope deviations of the mirror
- Developed fixtures to provide uniform back support to the entire shell during figuring and polishing
  - Stiff outer shell and a thin layer of backing/interface material that goes between the mirror shell and the outer support
    - High-viscosity liquids
    - Pitch
    - Granular materials - spherical glass beads

*Backing support system - A thin layer of backing material (not shown) acts as an interface between the mirror shell (red) and the stiff outer support clam-shell (gray).*





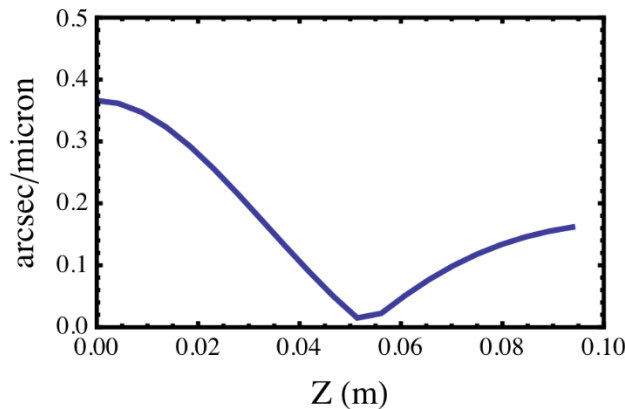


# Mounting Optimization

## Performance vs. Axial Mounting Location

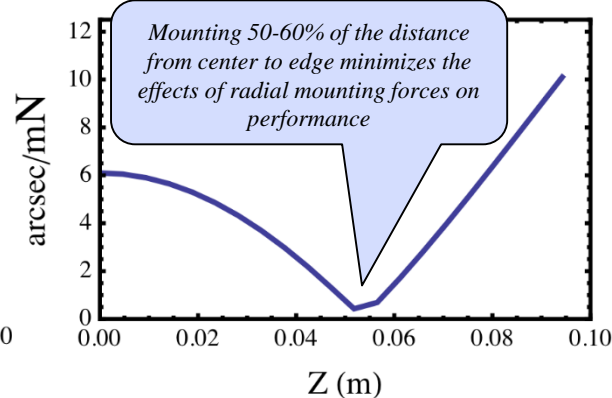
- The performance analysis of the cylindrical shell was performed, using both analytical methods and finite element analysis (FEA).
- Analytical methods were applied in Mathematica® and detailed finite element models (FEMs) were made in ANSYS.

2-Reflection RMS Angular Deviation per Unit Deflection vs. Axial Position of Applied Force

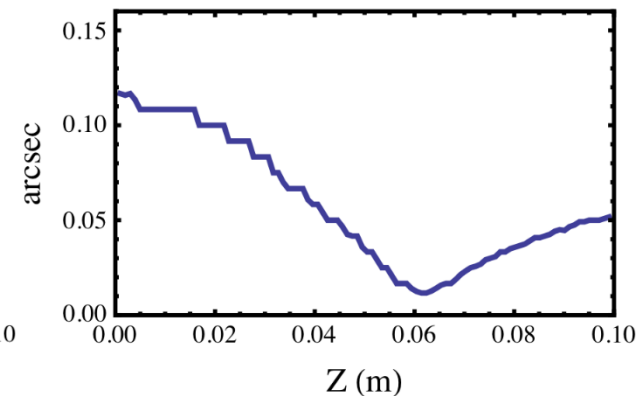


*Analytical models*

2-Reflection RMS Angular Deviation per Unit Force vs. Axial Position of Applied Force



2-Reflection HPD for 10 micron Deflection vs. Axial Position of Applied Force



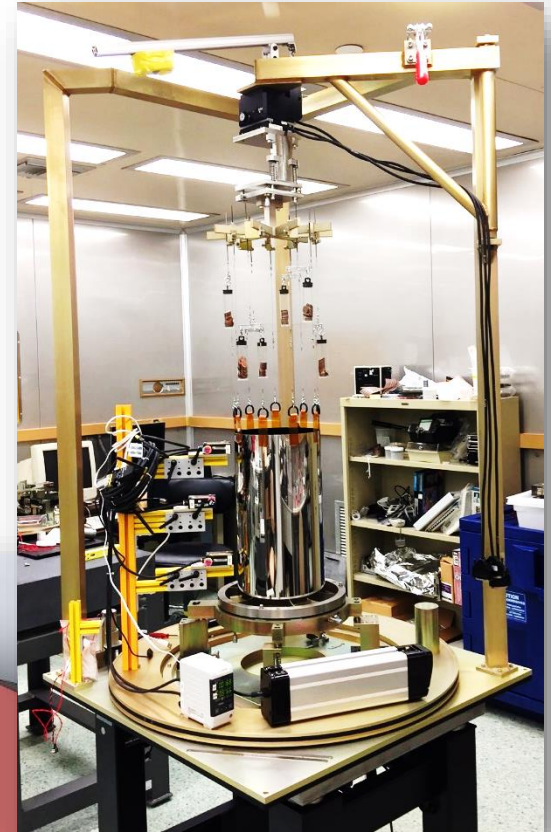
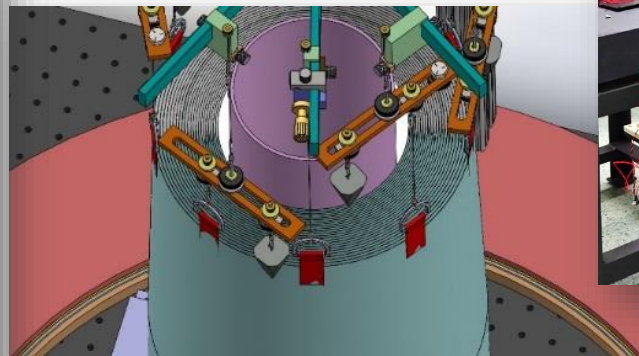
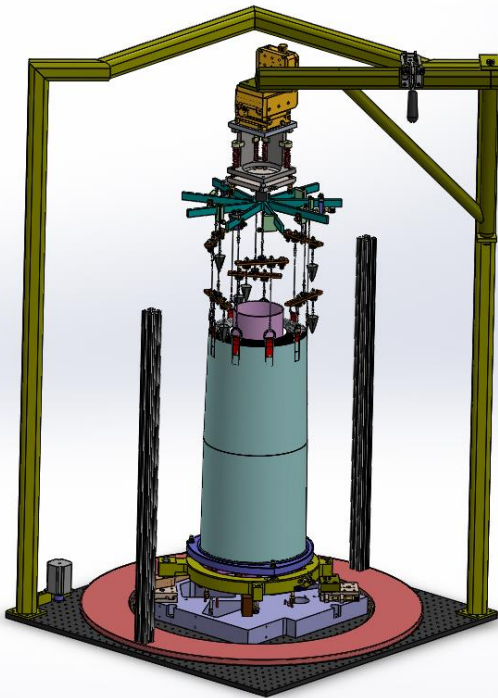
*FEA simulations*

Jacqueline M. Roche et.al, *Opto-mechanical analyses for performance optimization of lightweight grazing-incidence mirrors*. Proc. SPIE 8861, *Optics for EUV, X-Ray, and Gamma-Ray Astronomy VI*, 88611G (September 26, 2013); doi:10.1117/12.2026884.

# Alignment



- Strings approach – mirror is hung with strings
- Holding at the opposite end to the glue positions
- Equalizing the strings tension – self leveling and minimum distortions
- Off loading weight to the strings



# Metal – Ceramic Hybrid Shells

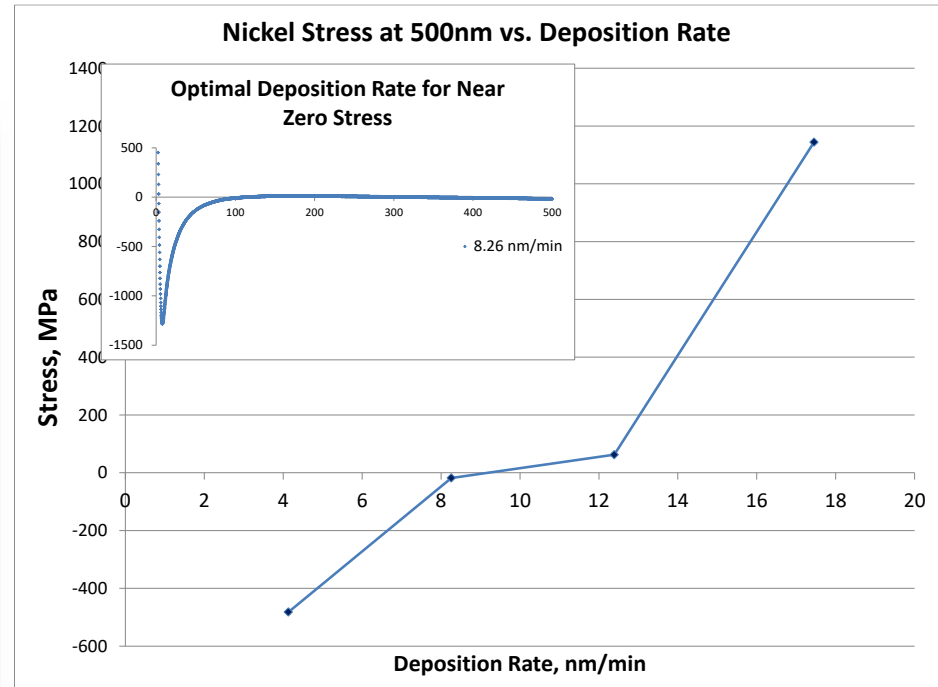
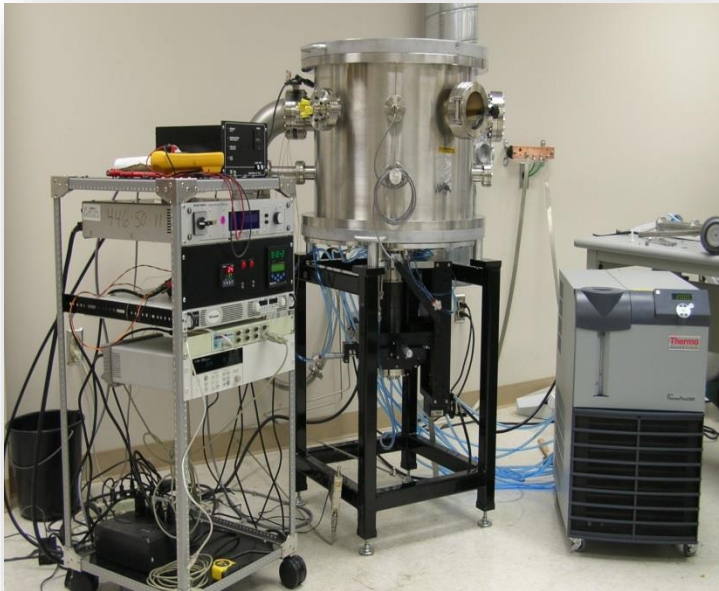


***Collaboration: NASA MSFC, SAO, ReliaCoat***

- Plasma thermal spray technology
- To replace the high density Nickel with light ceramic compound
- Ni density -  $8.9 \text{ g/cm}^3$ ; Ceramic compound density –  $\sim 2.5 \text{ g/cm}^3$
- Reduce the weight of the optic – keep the advantages of electroform nickel replication



# In-Situ Stress Measurement



*Preliminary measurements showing coating stress versus deposition rate at fixed gas pressure. Inset shows stress versus coating thickness (nm) at fixed deposition rate*



# Figure Correction: Differential Deposition

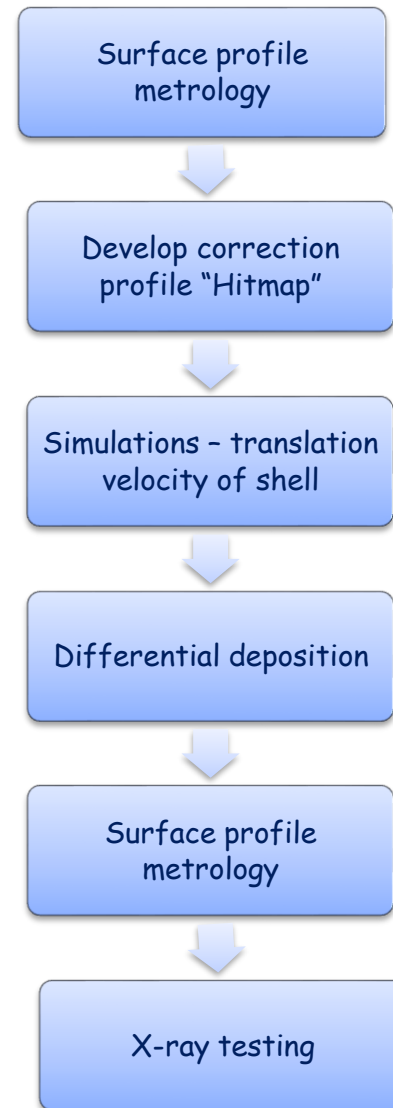
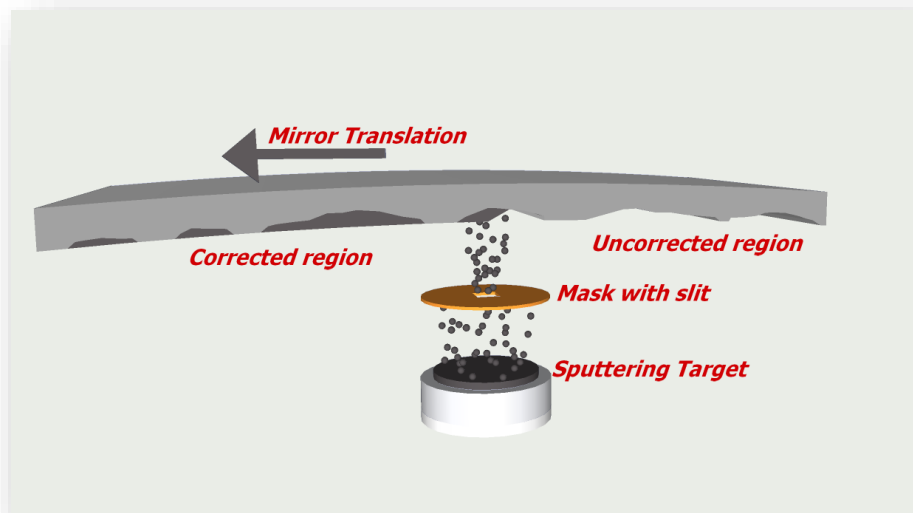


**What** Differential deposition is a technique for correcting figure errors in optics

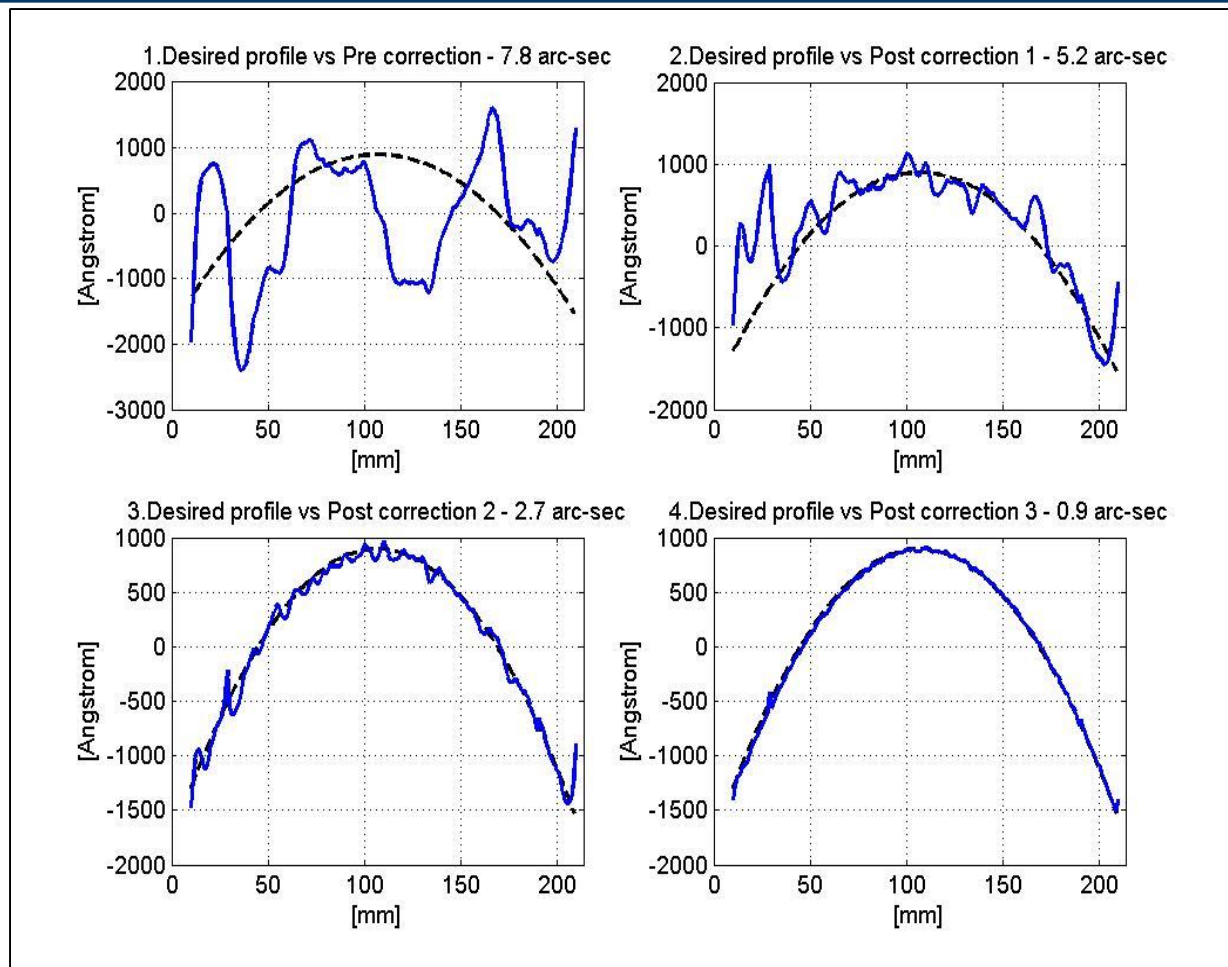
**How** Use physical vapor deposition to selectively deposit material on the mirror surface to smooth out figure imperfections

**Why**

- Can be used on **any type** of optic, full-shell or segmented, mounted or unmounted
- Can be used to correct a wide range of spatial errors. Could be used in conjunction with other techniques... e.g. active optics.

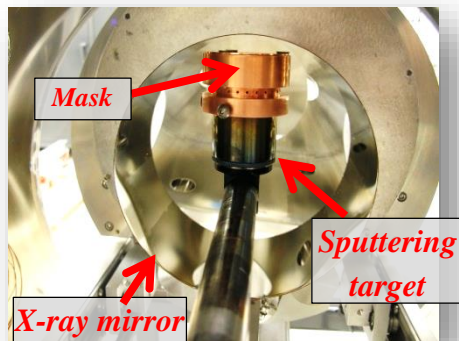
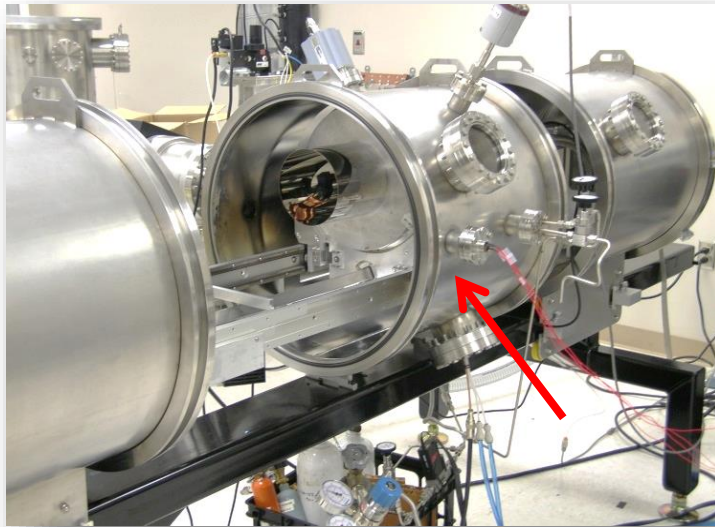


# Process Sequence – Differential Deposition

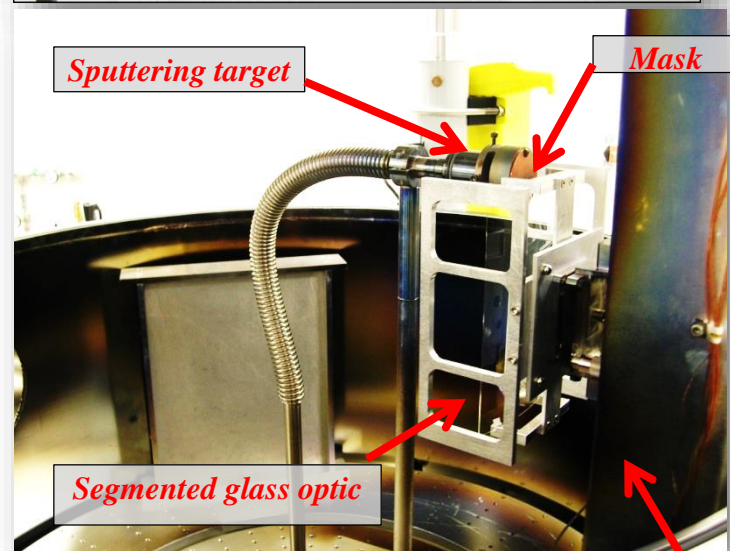


*Simulated correction sequence showing parabolic axial figure profile before (top left) and after 3 stages of correction using a beam of FWHM = 14mm, 5.2 mm and 1.7 mm respectively. The dotted line gives the desired figure and the solid line gives the figure obtained at each stage. Overall, resolution improved from 7.8 arcsec to 0.9 arcsec HEW (2 bounce equivalent).*

# Coating systems



*Sputtering head with copper mask positioned inside shell*

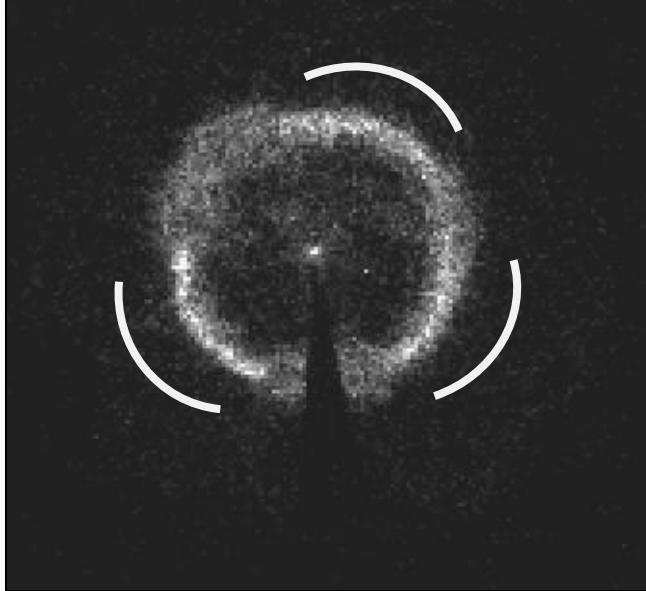


*Translation stage*

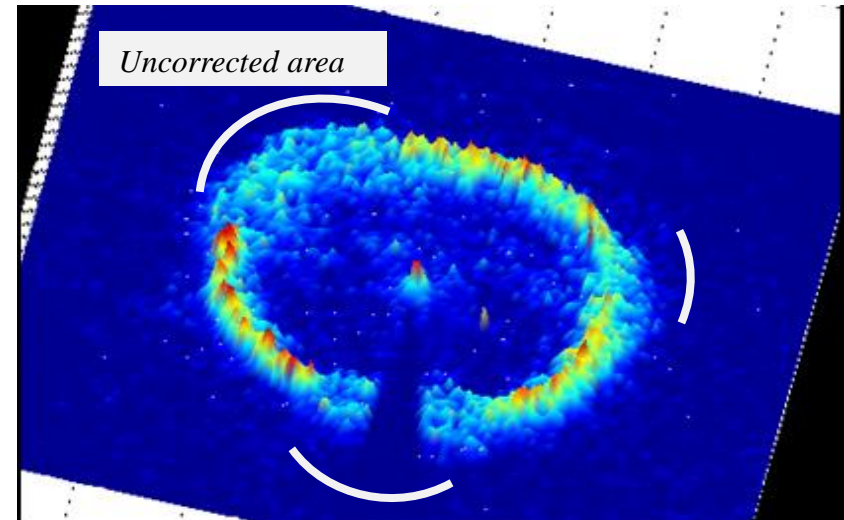
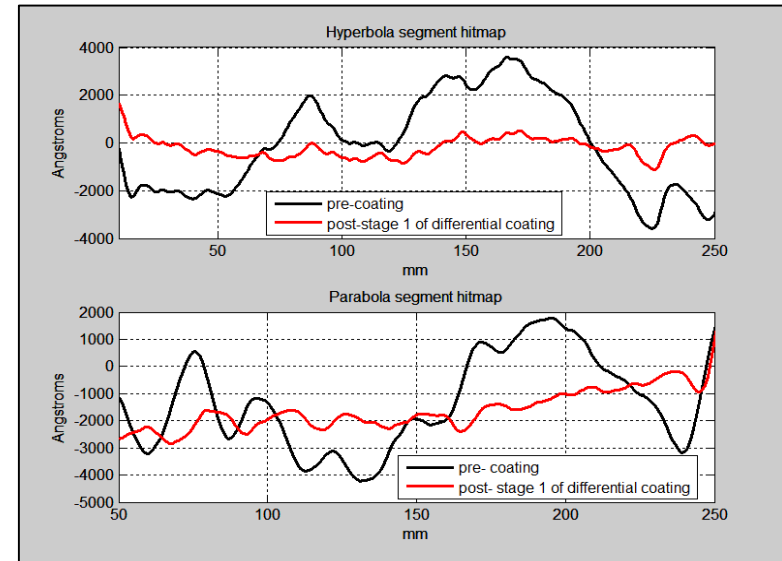
# X-ray testing – pre-and post- differential coating



*Marked areas - corrected azimuthal segments*



- Plots shows intra-focus X-ray image (-40 mm) of the corrected shell
- Corrected segments are visually obvious compared to the uncorrected in X-ray testing with the CCD

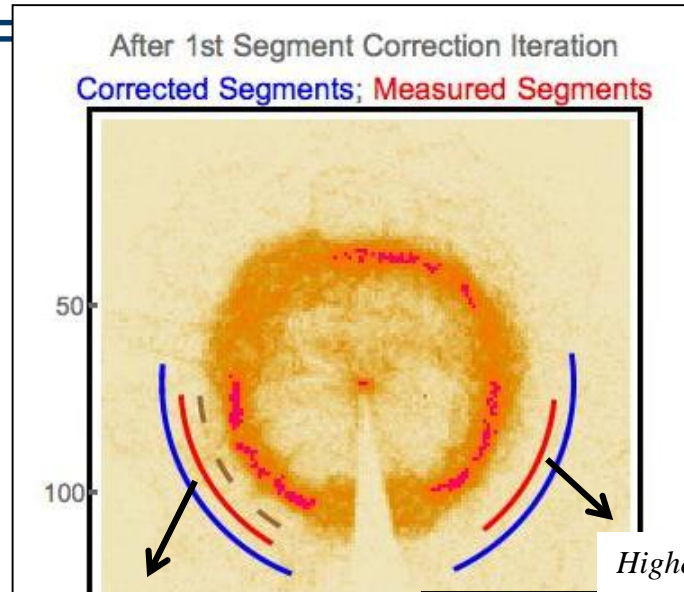




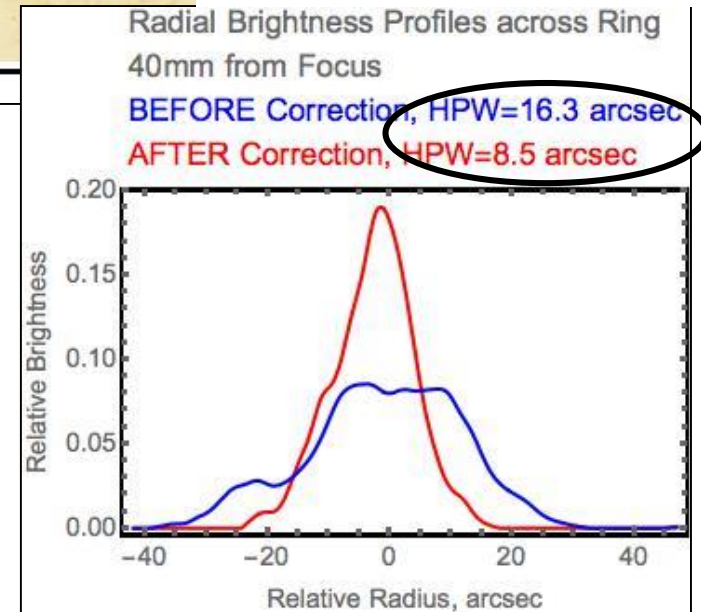
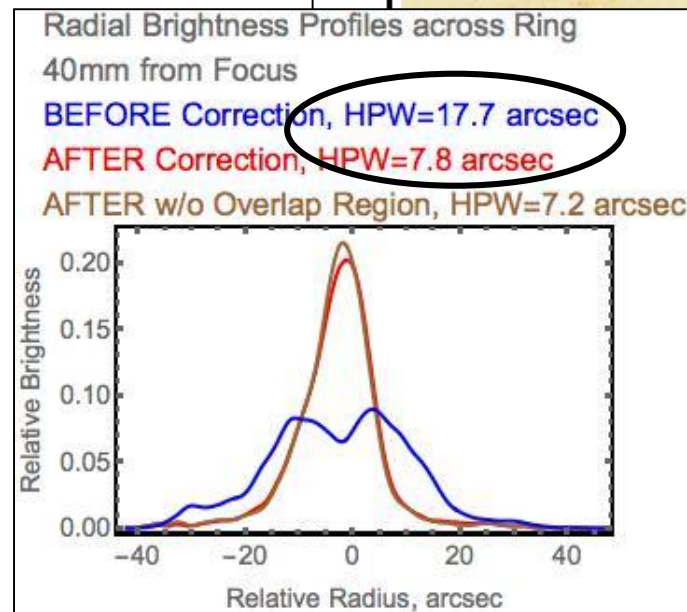
# X-ray testing – pre-and post- differential coating



A factor of >2  
improvement is  
achieved with one  
stage of correction



*Higher frequency- correction*



# Conclusion

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- Full-Shell Optics at MSFC
  - Electroform nickel replication has been used for past 20 years for satellite, rocket and balloon-borne missions and for various spin-off applications
- Improvements are underway
  - Better quality mandrels
  - Lower-stress electroforming
  - Direct fabrication (& polishing)
  - Post-fabrication figure correction
  - More precise alignment and assembly